

ZERO EMISSION TECHNOLOGIES : AN OPTION FOR CLIMATE CHANGE MITIGATION

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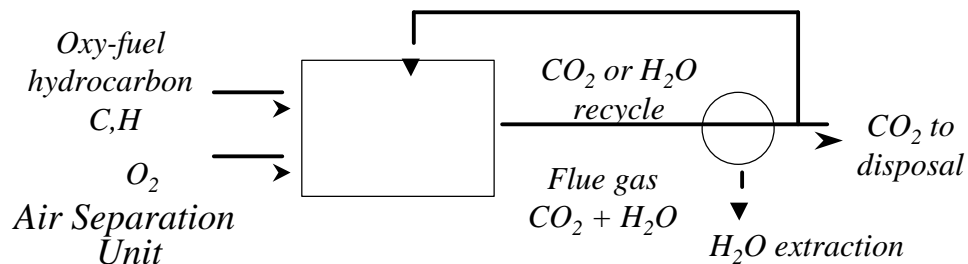
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Basic principle of a Zero-Emission Power Cycle (O₂/CO₂ or O₂ /H₂O cycles)

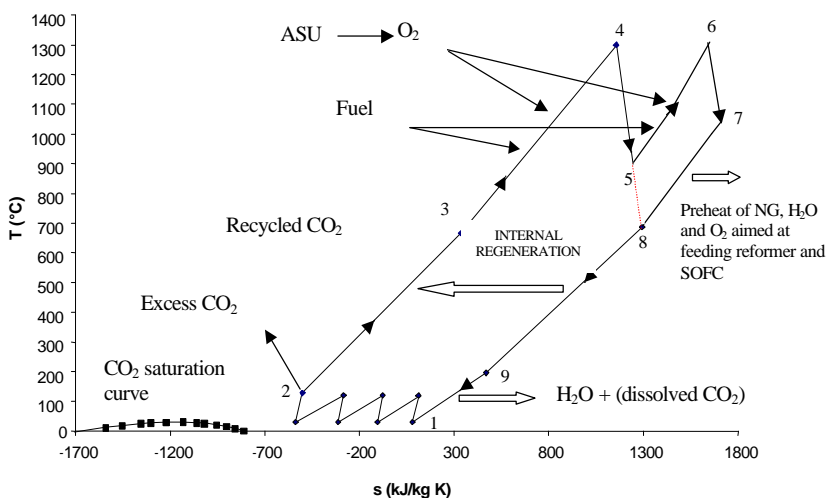


♦ O₂/H₂O and O₂/CO₂ : near Zero Emission Power Cycles
use of O₂ as the fuel oxydiser produced in an air separation unit
(ASU) and of H₂O or CO₂ as the cycle working fluid and thermal
ballast for flame temperature control

Rationale of oxy-fuel cycles for Near Zero Emission Power Generation

- Use of nearly pure O₂ (+ Ar) as fuel oxidiser so that the flue gas is highly enriched in CO₂ : **air separation required**
- Use of CO₂ itself or of H₂O as the working fluid in a gas cycle and as thermal ballast for flame t° control in stoichiometric proportions
- Separation of CO₂ and H₂O is easy and there is no longer need for a very penalising scrubber separating CO₂ from N₂ in the flue gas
- Take advantage of the performance of most advanced GTs
- Two main options
 - O₂/ H₂O cycles
 - O₂/ CO₂ cycles
- CES water cycle; Graz cycle; AZEP cycle (Alstom/NorskHydro); HiOx (Aker Kvaerner); MATIANT

The regenerative E-MATIANT gas cycle



1-2 : intercooled staged compressor ; 2-3 : upper pressure cycle ; 3-4 : HP combustion chamber ; 4-5 : HP expander ; 5-6 : LP combustion chamber ; 6-7 : LP expander ; 9-1 : water cooler/separator ; 4-5-8 : non reheated expansion.

Configurations of O₂/CO₂ MATIANT cycles

E-MATIANT cycle

Ericsson-like CO₂ regenerative gas cycle

Boundary conditions : TIT = 1300 °C; LP turbine exhaust gas : 700 – 750 °C complying with temperature limits of advanced materials in regenerator and HRSG

ASU, extracted CO₂, fuel and oxygen compressors in the system

Cooling of hot components with extracted CO₂ or with compressed N₂ from ASU

Pinch point at regenerator inlet : 100°C

Upper cycle pressure : > = 110 bar

Reheat pressure : optimised 25- 40 bar

Net cycle efficiency : 40- 45%

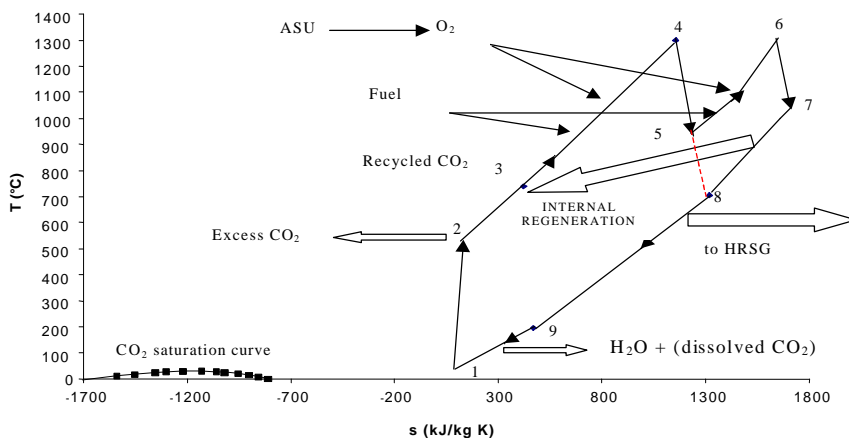
Improvements of O₂/CO₂ E-MATIANT cycles

- **Recycling** of the extracted water, superheated in the regenerator, in the LP combustion chamber: increase of specific power output and efficiency (similarly to STIG GTs)
- Use as a **CC**: adiabatic compressor and HRSG with advanced steam turbines (3PR, supercritical steam, 700°C) : ? > 50%
- Use as an **IGCC** : addition of a gasification unit and a syngas clean-up unit downwards of the GT combustion chambers. Asset: the ASU is already existing; no need for a shift reaction of CO in the syngas and separation of CO₂ and H₂ : ? ~42- 45%
- Integration of a high t° fuel cells **SOFC** by the use of the sensible heat in hot exhaust flue gas (900°C) for preheating of fuel, O₂ and water/steam : ? 47-49%
- Integration of a high t° conducting **membranes** (ITM or OTM) for oxygen production (900°C) : ? ~45%

Modelling of the cycles : CO₂ properties

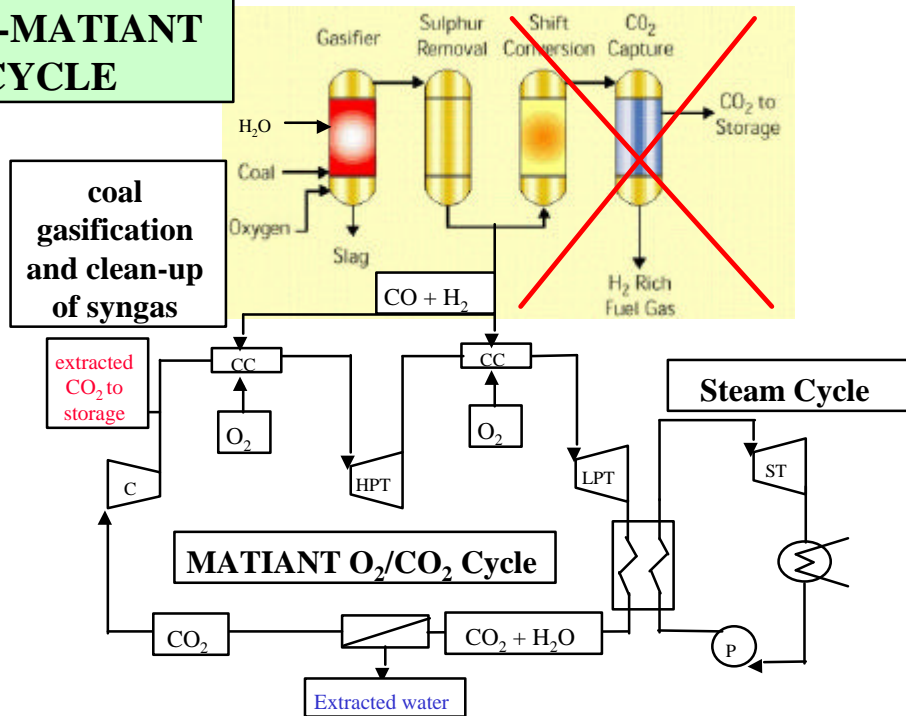
- Heavier than air and water (molecular weight: 44 against 29 and 18)
- Lower specific heat C_p than water (nearly the half) but roughly the same as air (for sizing of heat exchangers). Lower than air in the compression zone
- Lower adiabatic exponent $\gamma = C_p/C_v$ (for sizing of turbomachines): less compressible than air and steam
- Low critical point (73 bar; 31°C) against 221 bar; 375°C for water
- Higher density than water and lower in gaseous state than steam (influence on the dimensions of components)
- Chemically reactive (interaction with storage medium)
- **Supercritical CO₂ behaves like a liquid (density) and like a gas (viscosity)**

Combined Cycle based on a O₂/CO₂ Brayton-like gas cycle : CC-MATIANT cycle



Combined Cycle : O₂/CO₂ regenerative Brayton – like gas cycle with reheat and steam cycle with HRSG.
 1-2 : adiabatic compressor ; 2-3 : upper pressure cycle ; 3-4 : HP combustion chamber ; 4-5 : HP expander ;
 5-6 : LP combustion chamber ; 6-7 : LP expander ; 9-1 : water cooler/separator ; 4-5-8 : non reheated expansion.

IGCC-MATIANT CYCLE



COST OF CAPTURE or MITIGATION COST

⇒ Definition : ratio of increase of the electricity cost ΔCOE (c€/kWh) and of CO_2 emission reduction ΔE (g CO_2 /kWh)

⇒ MC (Mitigation Cost) = $\Delta\text{COE} / \Delta E$ (€/ton CO_2 avoided)

⇒ $\text{COE}_{\text{st}} = [I \text{ (capital cost/y)} + \text{O\&M/y} + F_{\text{st}} \text{ (fuel cost/y)}] / \text{PE (production/year)}$

$F_{\text{st}} = (\text{€/kWh}) = \text{fuel cost (€/GJ)} / \eta_{\text{st}} \text{ (kWh/GJ)}$

⇒ $\text{COE}_{\text{ZEP}} = [I \text{ (ZEP unit)} + \text{O\&M}_{\text{ZEP}}] \times [W_{\text{st}} / W_{\text{ZEP}}] + F_{\text{ZEP}} / \text{PE}$
 with $F_{\text{ZEP}} \text{ (€/kWh)} = \text{fuel cost (€/GJ)} / \eta_{\text{ZEP}} \text{ kWh/GJ} = F_{\text{st}} \times [W_{\text{st}} / W_{\text{ZEP}}] = F_{\text{st}} \times [\eta_{\text{st}} / \eta_{\text{ZEP}}]$

⇒ $E_{\text{ZEP}} = E_{\text{st}} \times (1 - R) \times W_{\text{st}} / W_{\text{ZEP}}$ ($R = 98\%$)

$\Delta E = E_{\text{st}} - E_{\text{ZEP}} = E_{\text{st}} [1 - (1 - R) \times W_{\text{st}} / W_{\text{ZEP}}]$

Reference NGCC $\eta_{\text{st}} = 55\%$; $E_{\text{st}} = 350 \text{ gCO}_2/\text{kWh}$

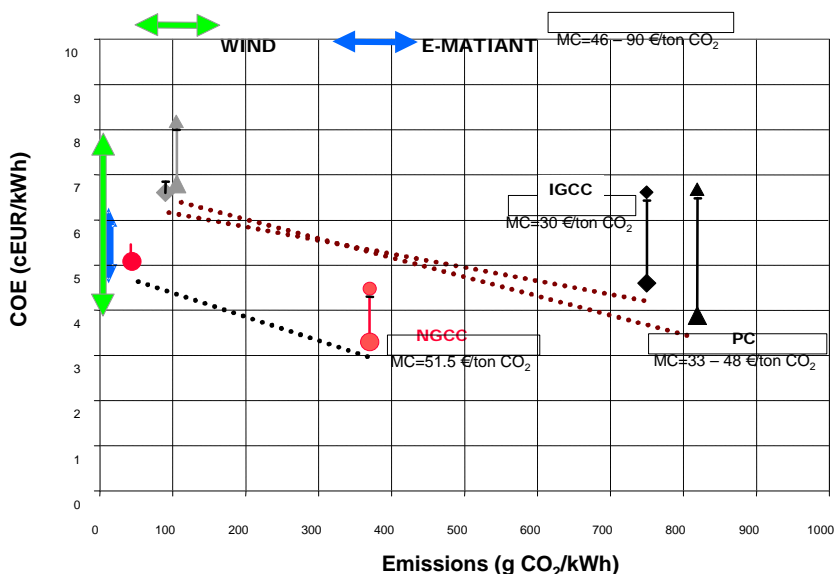
MITIGATION COST

**COE for a E-MATIANT plant 5 -7 cent€/kWh
+ 50-100% above the COE of a standard NGCC
Comparable to COE of wind energy (4-8 cent€/kWh)**

⇒ **MC : ranking of technologies with capture**

IGCC (30 €/ton CO₂ avoided) < PC (40.5+/-7.5) < NGCC(50.5)

⇒ **MC for the E-MATIANT cycle is 45 - 90 €/ton CO₂ avoided and is in the same range of that of natural gas and coal fired plants with capture by chemical absorption in the flue gas (40 - 60 €/ton CO₂ avoided)**



Cost of electricity COE (c€/kWh) versus specific emissions (gCO₂/kWh) for coal (PC, IGCC) and natural gas (NGCC, E-MATIANT) power plants without and with capture and without and with the external costs (vertical bars). The mitigation costs (the slope of the straight lines) are mentioned for each technology.

Technical issues in ZEP cycles

- The technical issues are linked to the composition of the working fluid: design of turbomachines operating on $\text{CO}_2 / \text{H}_2\text{O}$; development of materials and cooling techniques
- Cooling systems of CO_2 expanders and combustors at 1300°C and higher
- Combustion in pure O_2 in a CO_2 atmosphere under pressure, in stoichiometric conditions \rightarrow the flame stability is demonstrated at 1 bar
- Chemical behaviour of CO_2
- Oxygen production using high temperature membranes; chemical looping
- Development of high temperature steam turbines ($\geq 700^\circ\text{C}$) cooled with steam : steam cooled GT

Advantages of ZEP cycles

- Low emission of CO_2 AND of NO_x , SO_2 and particulates (lower than in flue gas and fuel decarbonisation)
- Separation of CO_2 and H_2O is easy in a cooler separator or a condenser
- Modular structure and low degree of complexity (availability and reliability)
- High fuel flexibility : fossil fuels, biomass and hydrogen
- Performance improvements by the use of advanced GTs and boilers
- Possible integration of high t° fuel cells and I TM at high t°

Advantages of ZEP cycles

- No use of chemicals for capture (no emission of solvents)
- No waste products (possibly toxic) to dispose of
- High purity of the delivered dry CO₂ (water separation); the extracted CO₂ is contaminated with non condensable gases (Ar, NO_x,N₂ coming from ASU and fuel) and with impurities from the fuel like sulfur, metals
- Potential for use at small and large scale in off- and on shore applications
- Cost constrain on the GT : purchase price has to be 200 €/kW as for a current advanced industrial air based GTs

Conclusions

- ZEP cycles are only designed for CO₂ emission mitigation but at the same time they do not release other pollutants. Then the question about CO₂ purity for the sequestration arises
- They accept a large range of fuels like solid and liquid fuels, NG, syngas CO + H₂, hydrogen, biofuels, wastes...for combustion or gasification
- The various types of ZEP cycles (O₂/H₂O and O₂/CO₂ MATIANT cycles) have high and similar performance (40-50% efficiencies) and very low specific emissions (a few gCO₂/kWh)
- Technical issues are solvable and ZEP cycles are feasible
- ZEP technology could be cost effective in a near future, especially in the framework of any kind of regulations on emissions and of fiscal measures (taxes, trading , certificates.)

FUTURE OBJECTIVES

- Need for cheap **O₂ production** (cryogenics; O₂ or ion transport through dense ceramic membranes; chemical looping; ceramic auto-thermal recovery(CAR); other)
- Need for **high efficiencies** and **cost reductions** in the long run by a **full integration**, especially of an air separation unit and of CO₂ re-use (EOR; ERCBM) and **sequestration**
- Need for **R&D,D** to demonstrate the concept in a **pilot plant by 2015**

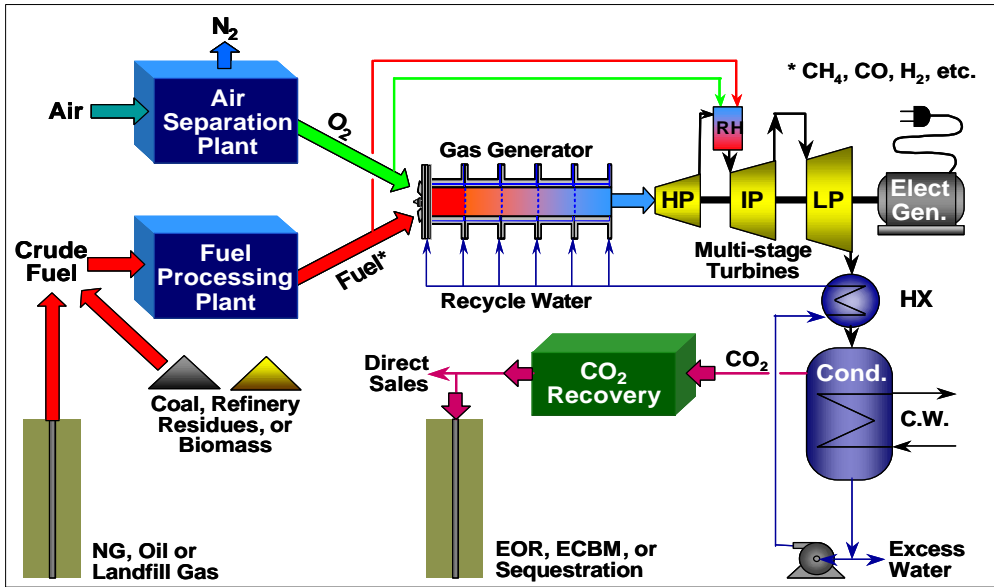
FUTURE PROSPECTS

- If **BIOMASS** (with reforestation) is used in co-combustion or co-gasification in ZEP plants, its carbon is separated and sequestered and is hence withdrawn from the carbon cycle : **negative emission**
- If a future economy is based on zero emission energy systems and uses **H₂** as an energy carrier, it has to be produced **free of carbon**, for instance by water electrolysis using zero emission plants (renewable energy, hydropower, nuclear energy, ZEPP), Then O₂ is simultaneously generated as a by-product.

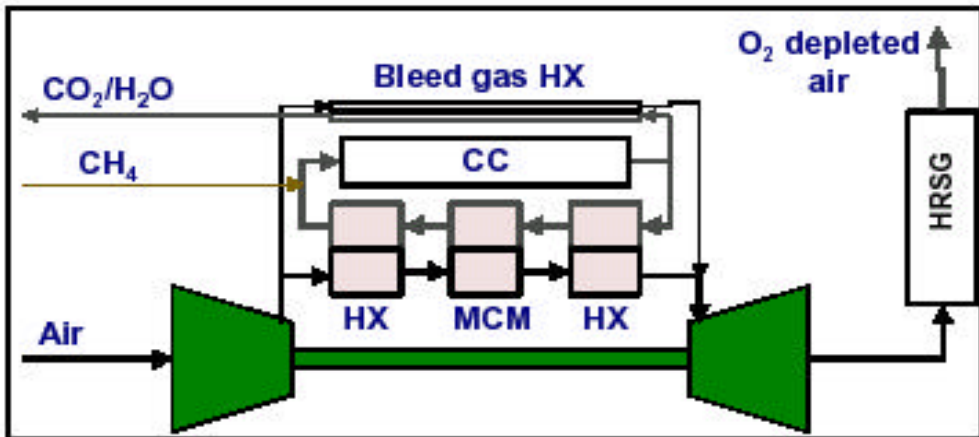
The real issue is to produce **cheap and clean H₂**

- High temperature **fuel cells** SOFC, renewable energies and sequestration technologies may be integrated in ZEP gas cycles, increasing efficiency and power output; but cost is currently prohibitive for fuel cells

The CES Process



Advances Zero Emission Power (AZEP) Process



Graz Cycle

